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# Development and performance evaluation of a novel dynamic headspace vacuum transfer "In Trap" extraction method for volatile compounds and comparison with headspace solid-phase microextraction and headspace in-tube extraction



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### ABSTRACT

Headspace in-tube extraction (HS-ITEX) and solid phase microextraction (HS-SPME) sampling, followed by gas chromatography-mass spectrometry (GC–MS), are widely used to analyze volatile compounds in various food matrices. While the extraction efficiency of volatile compounds from foodstuffs is crucial for obtaining relevant results, these efficiency of these extraction methods limited by their long extraction times and requirements for large sample quantity. This study reports on the development and application of a new extraction technique based on HS-ITEX hardware, which improves the extraction rate and capacity by operating under reduced pressure, called Dynamic Headspace Vacuum Transfer In-Trap Extraction (DHS-VTT). The results of the study indicate that DHS-VTT improves the extraction of the target compounds. The area of the mass spectrometer signal for each compound can be up to 450 times more intense than the HS-SPME and HS-ITEX techniques performed in the same experimental conditions of extraction temperature and time. DHS-VTT runs in automated mode, making it possible to work with smaller sample quantity and also favors the HS extraction of all volatile compounds. In addition, the necessary modifications to the installation were cheap and the life of an ITEX trap is up to 10 times longer than an SPME fibre.

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### 1. Introduction

In food and flavor analytics, maintaining sample quality is a significant challenge throughout the analytical workflow. A commonly used method for performing sampling of food is by headspace (HS) techniques. Although they are "clean" techniques with respect to the working environment and installations, from our experience they have several drawbacks depending on use such as: Extended heat treatment and extraction time, which can result in artifact formation, change of the molecular structure, and even degradation of the sample. Automated HS-microextraction sampling techniques perform extraction and injection into the gas chromatograph (GC) in a single step, but often result in a discriminative transfer of compounds from the sample into the headspace.

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Phase partition coefficients air-water (K<sub>aw</sub>), sorbent-air (K<sub>sorb-a</sub>), and sorbent-water (K<sub>sorb-w</sub>) are the three factors that influence the phase distribution during the extraction for a system in equilibrium [1]. Headspace solid-phase microextraction (HS-SPME) is a cheap, simple and sensitive automated technique for extracting volatile organic compounds (VOCs) from a complex matrix without specific sample preparation. However, our own experience shows that it is very difficult to make robust and accurate analytical methods using HS-SPME. To overcome certain drawbacks of HS-SPME, and add dynamic and automated features at the same time, 'in-tube extraction' (ITEX) was introduced in 2006 by CTC Analytics AG (Zwingen, Switzerland). The technique is generally operated using a multifunctional autosampler. HS-ITEX is a solventless dynamic HS microextraction technique derived from several other similar techniques (such as SPME and stir bar sorptive extraction (SBSE)) listed and described by Jochmann et al. [2]. HS-ITEX is a sequential extraction based on progressive dilution and extraction of the headspace on the sample. This extraction technique is related to the multiple headspace extraction method (MHE) [3-6]

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# Table 1GC/MS Detection Parameters for the Investigated Compounds and Validation Parameters of the DHS-VTT Method.

0.9989 0.9981 0.9996 0.9995 0.9965 0.9994	9.4 8.2 6.8 5.5 7.3	56.2 50.0	ti
0.9981 0.9996 0.9995 0.9965 0.9994	8.2 6.8 5.5 7.3	50.0	1
0.9996 0.9995 0.9965 0.9994	6.8 5.5 7.3		Q
0.9995 0.9965 0.9994	5.5 7.3	38.1	
0.9965 0.9994	7.3	26.8	
0.9994		58.8	ō
	6.5	23.0	h
0.9966	7.3	77.8	<u>→</u>
0.9999	4.9	69.3	
0.9994	7.8	23.1	
0.9999	7.8	31.9	
0.9994	8.4	48.4	
0.9999	7.4	40.6	1
0.9999	9.8	21.4	1
0.9962	14.5	60.4	ଦ
0.9999	13.2	23.8	e e
0.9988	4.7	45.5	P
0.9992	6.5	36.1	N
0.9991	3.0	72.9	
0.9993	14.0	23.6	
0.9987	11.0	18.2	
0.9939	2.2	55.1	
0.9994	15.5	19.6	1
0.9936	33.0	36.4	
0.9986	27.6	50.1	
0.9997	15.8	15.5	
0.9988	28.6	52.1	
0.9997	15.5	37.0	
0.9994	14.7	15.4	
0.9981	9.0	33.5	
0.9990	6.1	31.6	െ
0.9983	8.1	31.0	ro
0.9987	14.0	17.7	h h
0.9990	12.8	43.2	ω
0.9898	NA	10.7	1
0.9991	28.4	40.7	
0.9968	10.3	18.5	
0.9992	20.4	17.1	1
0.9997	6.9	45.5	1
0.9942	28.6	3.1	
0.9971	13.1	39.9	1
0.9985	NA	3.6	-
0.9987	43.8	25.3	
0.9901	9.4	1.0	
	0.9991 0.9968 0.9992 0.9997 0.9942 0.9971 0.9985 0.9987 0.9987 0.9901	0.9991         28.4           0.9968         10.3           0.9992         20.4           0.9997         6.9           0.9942         28.6           0.9971         13.1           0.9985         NA           0.9987         43.8           0.9901         9.4	0.9991         28.4         40.7           0.9968         10.3         18.5           0.9992         20.4         17.1           0.9997         6.9         45.5           0.9942         28.6         3.1           0.9971         13.1         39.9           0.9985         NA         3.6           0.9987         43.8         25.3           0.9901         9.4         1.0

NA: Not available.

and provides an interesting alternative to HS-SPME; it has been used to extract numerous volatile chemical compounds from various matrices, including food, plants, pollutants, and biological fluids [2,7-10]. Another similar technique developed by SmartNose SA (Marin-Epagnier, Switzerland), Inside Needle Dynamic Extraction (INDEX), uses the same concept of extraction as HS-ITEX, and further HS extraction techniques have been extensively reviewed in the literature [11]. Improvement of the different parameters of the HS-ITEX is required to achieve adequate signals through optimized extraction and thermal desorption [7,12]. The HS-ITEX key parameters are the nature of the sorbent material, the number of strokes (according to the literature: between 20 and 120 [2,3,8,10,13]), the extraction speed, the desorption speed, the sample, the trap and syringe temperature, and the headspace volume extracted. Many commercial extraction polymers were evaluated by Laaks et al. [14] and are available on the market. The trap can also be filled with noncommercial sorbents, such as multiwalled carbon nanotubes or polystyrene-divinylbenzene [1,9,15]. The choice of the sorbent material is made based on the target molecule to be extracted. An innovative technique developed by Barajas et al. [16] also makes it possible to evaluate and characterize sorbents by inverse gas chromatography column.

Depending on the matrix and desired results, improving different parameters may be required, making the optimization of the technology very complex compared to HS-SPME [17].

The goal of this study was to develop and optimize a reproducible, robust, and sensitive extraction method that reduces the drawbacks of traditional headspace extraction techniques. A new technique is proposed that combines features of HS-ITEX and principles of vacuum-HS-SPME and vacuum distillation coupled with gas chromatography [18–21]: Dynamic Headspace Vacuum Transfer In Trap Extraction (DHS-VTT). The new method aimed to avoid strokes, the limited injection volume and provide dynamic extraction under vacuum conditions. Several publications have reported a significant improvement of the extraction under reduced-pressure using so-called vacuum HS-SPME [22–24]. However, this technique can up to now only be used manually. To address this lack, the current method was designed to function with an automatic mode.

This paper discusses the development and application of our new extraction technique, DHS-VTT using a model of an artificially constructed matrix (ACM). We assess the method's sensitivity, and its suitability for the qualitative and quantitative analysis of a broad range of volatile compounds, small sample volume, and large sample series. The suitability and efficiency of DHS-VTT were verified by comparison to HS-SPME and HS-ITEX, as well as analysis of ACM and plain yoghurt using parameters commonly found in the literature for HS-ITEX and HS-SPME [25].

### 2. Experimental

### 2.1. Materials and methods

### 2.1.1. Chemicals and samples

The relevant chemical compounds were purchased from Sigma-Aldrich Chemie GmbH (Buchs, Switzerland), R.C. Treatt & Co. Ltd (Suffolk, United Kingdom), and Caesar & Loretz GmbH (Hilden, Germany): Hexan-1-ol (Aldrich 471402), 2-Phenylethanol (Aldrich 77861), Butan-2-one (Aldrich 360473), Butane-2,3-dione (Aldrich 885307), 3-Hydroxybutan-2-one (Aldrich W200808), Heptan-2-one (Aldrich W254401), Undecan-2-one (Aldrich W309311), Ethyl butanoate (Aldrich W242705), Ethyl 3-methylbutanoate (Aldrich W246301), Ethyl hexanoate (Aldrich W242906), Ethyl decanoate (Aldrich W243205), $\gamma$ -Butyrolactone (Aldrich 90970),  $\delta$ -Decalactone (Aldrich W236101), (Z)-6-Dodecen-4-olide (R.C. Treatt 62185), Butanal (Aldrich W221902), 3-Methylbutanal Table 2

Two-level full factorial design of experiment for the method validation.

Design	Sample temperature [°C]	Extraction time [min]
1	37	13
2	37	52
3	73	13
4	73	52
5	30	33
6	80	33
7	55	5
8	55	60
9	55	33
10	55	33
11	55	33
12	55	33

Changed parameters: sample temperature  $(37\,^\circ\text{C}\text{--}80\,^\circ\text{C})$  and extraction time (5–60 min).

(Aldrich 146455), Hexanal (Aldrich 115606), (E)-Hex-2-enal (Aldrich W256005), 2-Phenylacetaldehyde (Aldrich W287407), Nonanal (Aldrich W278203), (2E,4E)-Nona-2,4-dienal (Aldrich W321206), Acetic acid 99.7% (Aldrich 695092), Propanoic acid (Aldrich P1386), 2-Methylpropanoic acid (Aldrich W222208), Butanoic acid (Aldrich W222119), 3-Methylbutanoic acid (Aldrich W310212), 4-Methylpentanoic acid (Aldrich W346306), Hexanoic acid (Aldrich W255904), Octanoic acid (Aldrich W279927), Decanoic acid (Aldrich W+236411), Dodecanoic acid (Aldrich 61609), Pentane (Aldrich 236705), Hexane (Aldrich 296090), Heptane (Aldrich 246654), Octane (Aldrich 296988), Nonane (Aldrich 296821), Decane (Aldrich 457116), Undecane (Aldrich W510505), Dodecane (Aldrich 297879), Tridecane (Aldrich T57401), Tetradecane (Aldrich 172456), Pentadecane (Aldrich P3406), Hexadecane (Aldrich 296317), Polyethylenglycol 200 (Aldrich P3015), Miglyol 812 (Caesar 3274), Sodium chloride > 99% (Aldrich S9888), and phosphoric acid (Aldrich W290017). Plain yoghurt (3.5% fat) was purchased from a local supermarket.

### 2.1.2. ITEX sorbent materials

ITEX traps filled with Tenax<sup>®</sup> TA (TTA), Tenax<sup>®</sup> GR (TGR), Cabosieve S III (CSIII), and Cabosieve S III/Tenax<sup>®</sup> TA (CSIII/TTA) were purchased from BGB Analytik AG, Boeckten, Switzerland.

### 2.1.3. Artificially constructed matrix (ACM)

To develop and optimize the DHS-VTT technique, a stable sample was prepared using 43 target compounds representing chemical families that are often present in dairy matrices (alcohols, ketones, aldehydes, alkanes, carboxylic acids, and lactones; see Table 1), all diluted to a concentration of  $10 \text{ mg L}^{-1}$  in 20 mL of polyethylene glycol 200. The alkanes were separately diluted in Miglyol<sup>®</sup> 812 at the same concentration. Polyethylene glycol 200 was chosen because it is a good solvent for the selected compounds and does not react with the volatile compounds present in the ACM. The compounds that are not soluble in polyethylene glycol 200 (the alkanes) were dissolved in Miglyol<sup>®</sup> 812 which also simulates the lipid part of a dairy matrix. These mixtures were stored at  $-40 \,^\circ$ C until analysis.

### 2.1.4. Sample preparation

ACM standard solutions  $(25 \,\mu\text{L}\text{ of each standard})$  was diluted with  $H_3PO_4 4\%$  in deionized water at pH 1.3 (total sample volume of two millilitres) and placed in 20 mL HS vials (Interchim, Montluçon, France). The acidification of the sample helps to promote the volatility of carboxylic acids. Phosphoric acid is not volatile and will not interfere in the analyses either. The vials were hermetically sealed using a blue silicone/Teflon septum (Interchim). Calibration curves were made by diluting the stock solution by a factor of two for a minimum of seven points. To facilitate data processing, the 43

# Table 3

Comparison between DHS-VTT with different sorbent materials, HS-ITEX TTA and HS-SPME for the investigated compounds.

	HS-ITEX TTA	HS-SPME DVB/CAR/PDMS 1cm	DHS-VTT CSIII	DHS-VTT TGR	DHS-VTT TTA	DHS-VTT TTA/CSIII	
Pentane	1 7E+05	ext. time 30 min at 55°C	ext. time 30min at 55°C	ext. time sumin at 55°C	ext. time sumin at 55°C	ext. time sumin at 55°C	
Hexane	3 2E+05	3.0E+05	4 6E+05	1 9E+04	5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4	5.8E+05	
Hentane	3.2E+05	6.9E+05	1.7E+06	1.3E+06	5.2E+05	3.8E103	
Octane	4.0E+05	1.0E+06	4.3E+06	4 6E+06	5.2E+06	5.4E+06	
Butanal	8 6E+05	2.3E+05	1.2E+06	2 7E+05	3 6E+05	9 2E+05	្ន
Nonane	5.3E+04	7.3E+05	1.4E+06	1.5E+06	3 2E+06	2 9E+06	oup
Butan-2-one	1 1E+06	1.2E+06	3 2E+06	3 1E+05	2 3E+04	4 1E+06	-
3-Methylbutanal	1 0E+05	1 1E+05	1.2E+05	8.6E+04	2.5E+04	1 2E+05	
Decane	2 1E+04	1.3E+05	9.2E+05	1 1E+06	3.4E+06	3.3E+06	
Butane-2.3-dione	2.0E+05	2.3E+05	1.1E+06	4.7E+05	6.6E+05	1.4E+06	
Ethyl butanoate	2 8E+04	1 8E+05	7.4E+05	6.2E+05	1 1E+06	1.0E+06	
Ethyl 3-methylbutanoate	2 2E+05	7 7E+05	1 1E+07	9.2E+06	1 5E+07	1.4E+07	
Undecane	1 2E+04	3 9E+04	3.8E+05	6.7E+05	2 7E+06	2.8E+06	
Hexanal	1 6E+05	5.7E+05	8.9E+05	1.8E+06	2.6E+06	1.8E+06	0
Dodecane	7 0E+03	4 1E+04	1.0E+05	3.8E+05	1 6E+06	1.8E+06	irou
Heptan-2-one	2 6E+04	2 7E+05	1.5E+06	1.5E+06	3 1E+06	3 2E+06	ıp 2
Ethvl hexanoate	1 8E+04	5.3E+05	1.1E+06	1.4E+06	2 6E+06	2 7E+06	
(E)-Hex-2-enal	3.8E+04	2.9E+05	5.3E+06	4 2E+06	1.0E+07	1.0E+07	
Tridecane	3.4E+03	2.0E+04	2.3E+04	2 2E+05	8.3E+05	1.0E+06	
3-Hvdroxy-butan-2-one	0.0E+00	1 4E+03	1.6E+04	6.8E+04	1.3E+05	7 4E+04	
Hexan-1-ol	1 9E+04	1.5E+05	8.9E+05	6.7E+05	1.3E+06	1 2E+06	
Tetradecane	6.4F+02	9 4F+03	5.6E+03	1.3E+05	3 9E+05	5 0E±05	
Nonanal	1 4F+04	1 1E+05	3.2E+05	2 2E+06	2 8E+06	3 0E+06	
Acetic acid	0.0E+00	1.1E+05	7.2E+05	1.6E+06	6.4E+05	2 4E+06	
Pentadecane	0.0E+00	5.7E+03	2.9E+03	6.5E+04	1.7E+05	2.3E+05	
Propanoic acid	1.5E+04	1.1E+05	1.6E+06	2.3E+06	2.4E+06	5.0E+06	
Hexadecane	0.0E+00	6.8E+04	2.0E+06	2.9E+06	3.3E+06	4.2E+06	
2-Methylpropanoic acid	0.0E+00	1.7E+03	3.4E+03	3.9E+04	7.1E+04	1.1E+05	
Undecan-2-one	3.8E+02	4.0E+03	6.5E+04	3.9E+05	4.6E+05	8.0E+05	
Butanoic acid	2.1E+04	5.0E+05	8.2E+06	1.0E+07	1.6E+07	2.4E+07	
Ethyl decanoate	1.6E+03	1.7E+04	7.2E+04	7.3E+05	6.4E+05	1.4E+06	Gr
3-Methylbutanoic acid	1.9E+04	6.4E+04	1.8E+05	1.6E+06	3.2E+06	2.4E+06	dnc
2-Phenylacetaldehyde	0.0E+00	1.8E+04	2.8E+05	2.3E+05	3.2E+05	3.3E+05	ω
y-Butyrolactone	1.8E+03	1.4E+05	4.9E+06	6.3E+06	9.4E+06	1.1E+07	
(2E,4E)-Nona-2,4-dienal	0.0E+00	3.5E+03	7.2E+04	5.9E+05	1.1E+06	1.6E+06	
4-Methylpentanoic acid	0.0E+00	4.0E+04	5.6E+05	1.3E+06	2.5E+06	3.4E+06	
Hexanoic acid	0.0E+00	6.9E+04	5.5E+05	1.2E+06	2.8E+06	3.7E+06	
2-Phenylethanol	0.0E+00	2.2E+05	2.8E+06	3.8E+06	7.1E+06	7.9E+06	
Octanoic acid	6.1E+03	5.8E+04	2.1E+04	2.6E+05	3.9E+05	5.3E+05	
δ–decalactone	0.0E+00	0.0E+00	5.5E+03	1.3E+04	1.1E+04	5.2E+04	
Decanoic acid	7.7E+02	8.8E+03	1.8E+04	8.5E+04	3.6E+04	4.7E+04	
(Z)-6-Dodecen-4-olide	0.0E+00	0.0E+00	6.1E+03	1.3E+04	1.4E+04	1.7E+04	
Dodecanoic acid	0.0E+00	0.0E+00	1.3E+04	8.0E+03	4.0E+03	4.4E+03	

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The values represented are the total ion count (TIC) [-] for the MS signal

compounds were classified into three groups, based on their molecular weight and volatility as well as elution time: group 1, spanning over C5 and C10; group 2, spanning over the first peak right after C10 and C13; and group 3, spanning over the first peak right after C13 and C20 (Tables 1 and 3).

For real dairy analyses, two millilitres of homogenized plain yoghurt were placed in 20 mL HS vials (Interchim) and they were hermetically sealed using a blue silicone/Teflon septum (Interchim).

### 2.1.5. Modification of the gas distribution block

The original two-way aluminum gas distribution block of the autosampler MPS2 (Gerstel, Sursee, Switzerland) was replaced by a three-way block printed on a 3D Touch Pegasus printer (Full Spectrum Laser, Las Vegas, US) with "Universal Clear Resin" (Full spectrum Laser) (Fig. 1). The polymer was solidified using UV exposure after printing. This modification makes it possible to switch the solenoid valve between the vacuum pump and the inert gas to extract volatile compounds from the sample with the vacuum and desorb them into the injector using an inert gas flow.

#### 2.1.6. Pressure measurement

In order to verify the hermeticity of the vial, a pressure of 10 mbar was applied in an empty vial using a vacuum pump Buchi V-300 equipped with a pressure control interface I-300 (Büchi, Flawil, Switzerland). The vial was connected to a pressure sensor PAA-27 (Keller, Winterthur, Switzerland) and a measuring device Almemo 2590 (Ahlborn, Holzkirchen, Germany). The pump was then stopped and the signal was recorded simultaneously in a csv file and processed with Excel.

Evaluation of the pressure in the vial during HS-ITEX and DHS-VTT extraction was carried out using the same equipment as described above. The measuring device was connected to a needle which pierces the septum of the vials at the same time that the extraction was performed. Instrumentation for GC–MS analysis

The analyses were completed using an MPS2 autosampler (Gerstel) on an Agilent 7890B GC system coupled to an Agilent 5977A mass selective detector (MSD) (Agilent Technology, Santa Clara, CA, USA). The headspace was extracted according to the experimental design (Table 2). Bound volatiles were desorbed in a PTV of type CIS 4 (Gerstel). Volatile compounds were separated on a TRB-FFAP fused silica capillary column (100% PEG with nitroterephthalic acid, bonded and crosslinked, 60 m × 0.32 mm × 1.0  $\mu$ m film; Teknokroma, Barcelona, Spain) with helium as the carrier gas at a constant flow of 2.5 mL min<sup>-1</sup> (30 cm sec<sup>-1</sup>).

The oven temperature program was as follows: five minutes at 40 °C, then heated to 220 °C at a rate of 5 °C min<sup>-1</sup>, with a final hold time of 34 min to make a total run time of 75 min. The MS settings were as follows: the transfer line at 230 °C, the source temperature at 230 °C, the compounds monitored in SCAN mode between 29 amu and 250 amu without solvent delay, and in SIM mode for the method detection limits (MDLs) and the calibration curves. The autosampler was controlled using the Cycle Composer V. 1.5.4 (CTC Analytics, Zwingen, Switzerland) and the PTV injector with Maestro1 software V.1.4.8.14/3.5 (Gerstel). The detector response signals were integrated using Masshunter quantitative analysis software version B.08.00 (Agilent). The NIST/EPA/NIH mass spectral library (NIST14) version 2.2 (NIST, Gaithersburg, MD, USA) was used for peak identification.

### 2.2. Headspace in-tube extraction (HS-ITEX)

The ITEX-2 option (Brechbühler, Schlieren, Switzerland) was used on the MPS2 autosampler. The headspace was extracted using a TTA trap with 70 extraction strokes (volume of 1.3 mL/stroke, extraction flow rate of 100  $\mu$ L s<sup>-1</sup>). ACM and yoghurt samples were

not conditioned for this experiment. The syringe temperature was fixed at 100 °C, the ITEX trap at 35 °C, and the sample at 55 °C. The bound volatiles were desorbed from the sorbent material at 240 °C in a CIS4 injector equipped with a glass liner filled with TTA at 10 °C. A volume of 1.3 mL was transferred into the injector at a desorption flow rate of 100  $\mu$ Ls <sup>-1</sup>, after having waited 30 s (plunger down) in the vent mode (50 mL min<sup>-1</sup>, set pressure: 0 kPa). The injector was then heated at a rate of 12 °C s <sup>-1</sup> to 240 °C. The purge flow to split vent was set at 300 mL min<sup>-1</sup> after 5 min. After injection, the ITEX needle was reconditioned according to the supplier's temperature recommendation for 15 min under a nitrogen flow of 220 mL min<sup>-1</sup> (measured at 35 °C).

## 2.2.1. Headspace solid-phase microextraction (HS-SPME)

To obtain a representative evaluation of the VOCs of the samples, the VOCs were extracted using a 1 cm 50/30  $\mu$ m divinylbenzene/carboxen/polydimethylsiloxane (DVB/CAR/PDMS) StableFlex fibre (Supelco, Bellefonte, PA, USA). The fibre was conditioned according to the supplier's recommendations (270 °C for 60 min). ACM and yoghurt samples were not conditioned for this experiment. The sample headspace was extracted for 30 min at 55 °C with an agitation rate of 250 rpm. The bound volatiles were desorbed for 60 s at 240 °C in the injector, which was in the splitless mode for 60 s before the split valve was opened (split flow =80 mL min <sup>-1</sup>) [25].

# 2.2.2. Dynamic headspace vacuum transfer in trap extraction (DHS-VTT)

DHS-VTT requires the same equipment as HS-SPME and HS-ITEX methods. A vacuum pump with pressure control interface and the new gas distribution block complete the installation (Fig. 2 A).

A piece of cleaned swab Topper<sup>®</sup> 8 10  $\times$  10 cm (Systagenix, North Yorkshire, United Kingdom) was added to the vial to avoid boiling and foaming. The syringe temperature was fixed at 100 °C, the ITEX trap at 35 °C, and the sample according to the experimental design (Table 2). The extraction takes place as illustrated (Fig. 2B). Sample conditioning: ACM and yoghurt samples were not conditioned for this experiment. Extraction: The trap pierces the septum and the plunger rises to the upper position. When the plunger is in the upper position, the HS was extracted under continuous reduced pressure using a vacuum pump Buchi V-300 equipped with a pressure control interface I-300 (Büchi) and the gas distribution block according to the experimental design (Table 2) without agitation. Drying: The trap was then removed from the sample and the solenoid valve switches to nitrogen. Sorbent and syringe were dried under a nitrogen stream for 17 min at 220 mL min <sup>-1</sup> [26]. Desorption: The trap was then introduced into the PTV injector and the bound volatiles were desorbed from the sorbent for 120s with a nitrogen flow of 220 mL min<sup>-1</sup> (fixed at 35 °C) at 240 °C. The PTV injector was in the vent mode at  $50 \,\text{mLmin}^{-1}$  and  $0 \,\text{kPa}$  for  $120 \,\text{s}$ . The injector was equipped with a glass liner filled with TTA and cooled with liquid nitrogen at 10°C. The trap was removed from the injector and the injector was then heated, at a rate of  $12 \circ C s^{-1}$ , to 240 °C. The purge flow to split vent was set at 300 mL min<sup>-1</sup> after 5 min. Trap Cleaning: The reconditioning of the trap was achieved in the same way as for the HS-ITEX method by circulating a flow of nitrogen through the trap at the recommended temperature with the plunger in the upper position.

### 2.3. Experimental design and statistics

To optimize experimental parameters, a two-level full factorial design of the experiment was performed. Only the sample temperature and the time of extraction were investigated because these are the parameters that have the most easily modifiable and have the greatest impact on the extraction of volatile compounds. The temperature of the trap should be kept as low as possible



Fig. 1. Design of the modification of the gas distribution block in polymer (dimension in mm). The block was designed with three ways, one for the nitrogen supply (A), one for the vacuum (B), and the last way was directly connected to the autosampler.



Fig. 2. (A) Diagram of the GC–MS instrument with the autosampler (MPS2) and ITEX-2 hardware. Connection of the original nitrogen line to the new distribution block (in orange) and the solenoid valve. The vacuum and nitrogen lines are coloured green and blue respectively. (B) Stages of the extraction process using the DHS-VTT method. Sample conditioning, extraction, drying, desorption and trap cleaning steps.



Fig. 3. Parameter optimization according to the experimental design for DHS-VTT (TTA/CSIII). X-Axis: Sample temperature [°C]. Y-Axis: Extraction time [min]. Z-Axis: Total ion count normalized [-]. The color variations represent blue for a low signal and red for a high signal.

(within the constraints of the instrument specifications and the laboratory environment) and the syringe temperature kept at 100 °C to exclude water condensation during the extraction. Three centrally composed DHS-VTT experimental plans were developed. The respective results were evaluated and presented to show the areas of effect. Mosaic plots (Fig. 3), which can be interpreted using color, were chosen for the present work, and each peak area of effect was smoothed squarely (smoothing method). In the plots, the intensity of the peak area observed is displayed in color, from blue (no signal), through dark and light green, yellow-orange, and, finally, to red, the largest and most intense peak area, which is equivalent to the maximal signal. The mean values of these measurement ranges were the center of the Central Composite design. The remaining levels were placed radially around the center in a 2 \* 2<sup>2</sup> experiment, which corresponds geometrically to two squares, rotated by 45° in the plane around their center. This design allows for the influence of five levels per parameter. Height points are distributed around the center at the same relative distance. In total, 12 measuring points are made, the center point for the variability being measured four times.

# 3. Results and discussion

### 3.1. Extraction parameters

### 3.1.1. Pressure in the headspace

The effectiveness of blue silicone/Teflon septum in the hermeticity of vials has shown that the pressure remained stable for a period of 10 min after the pump was stopped and thus can be considered as sufficiently effective for the analyses (results not shown).

The pressure measurements made during the extraction according to the HS-ITEX method show that the extractions were carried out above atmospheric pressure due to air expanding in the vial during extraction when it was heated. The sample was prepared at atmospheric pressure before extraction then placed in the autosampler cooling device (4 °C). The pressure immediately decreased due to the volume contraction of the air in the vials. Then the vial was placed in the heating agitator (55 °C), and the pressure increased above the atmospheric pressure (Fig. 4, red signal). Throughout extraction, the high pressure remained constant. As a result, the rate of evaporation of the compounds decreases and the extraction efficiency of volatile compounds was thus lower [27].

This phenomenon was similar during an HS-SPME extraction without the strokes effect. With the change of the gas distribution block, it was possible to automate the extraction at reduced pressure in the vial throughout the extraction (Fig. 4, green signal). The



Fig. 4. The pressure inside the vials during extraction using HS-ITEX (red) and DHS-VTT (green) method at set pressure: 100 mbar.

vacuum obtained in the vials greatly influenced the extraction of volatile compounds [22]. A pressure above 100 mbar was no longer sufficient for extracting the compounds efficiently (Fig. 5). Reduced pressure accelerated the release of the volatile compound in the headspace, but also has an impact on the efficiency of the sorbent. Low pressure over a long period of time desorbs the most volatile compounds of the sorbent. Consequently, it was necessary to determine the optimal conditions for achieving a suitable compromise between the pressure in the vial and the extraction rate. The pressure effects depended on the volatility of the molecules. The highly volatile compounds as the pentane were better retained on the polymer when the pressure in the vial was not less than about 50 mbar (data not shown), while other volatile compounds were more easily extracted at the lowest possible pressure. The effect of the reduced pressure during extraction caused an issue already known from the purge and trap technology-the accumulation of water vapor in the system (needle, syringe, tubes) and artifact formation [12,26]. To avoid this, the trap and the syringe were dried under a nitrogen flow for a time determined prior to injection into the injector.

### 3.1.2. Sample volume and HS volume

Tests were conducted using sample volumes of 0.5, 1, 2 and 4 mL in 20 mL HS vials. The DHS-VTT parameters were the same



Fig. 5. The sum of the peak areas of the 43 target compounds divided into three groups (Y-Axis: Total ion count) as a function of the pressure in the vials, expressed in mbar (set pressure) (X-Axis).



**Fig. 6.** Influence of the sample amount on the total ion count (TIC) MS signal of the target compounds.

for each test. The amount of the sample, and, consequently, the number of volatile molecules available in the vials influenced the extraction. When the amount of the sample doubled, the total signal increased proportionally by a factor of 1.7 for a given extraction time (Fig. 6). This demonstrates that the extraction capacity of the

trap was not reached, allowing for quantitative studies using a 2 mL sample [28,29].

### 3.1.3. PTV injector temperature

Low temperature in the liner had a positive impact on the recovery of volatile compounds. The change from  $10 \degree C$  to  $-50 \degree C$  does not show a significant improvement in recovery of volatile compounds for groups 2 and 3. For reasons of cost and efficiency, we used a temperature of  $10 \degree C$  for the PTV (Fig. 7).

## 3.1.4. Sample temperature and extraction time

The effect of the sample temperature was evaluated for temperatures between 30 and 80 °C using the described experimental design (Table 2). Increased temperature led to an increase in the signal for all compounds due to a higher partitioning of compounds from the aqueous phase to the headspace [1]. The higher the temperature, the higher the extraction efficacy for the less volatile compounds. At certain high temperatures, the compounds degraded and tended to contaminate the autosampler, i.e., water vapor condensed in the trap, the syringe, and the autosampler tubes. Despite the hydrophobic nature of TTA, an accumulation of water in the trap could result in the problem of injecting water droplets into the GC with the injection of the compounds [26].



Fig. 7. Influence of the PTV injector temperature on the recovery of the investigated compounds after injection. The injector temperature was tested between 20°C and -50°C.



**Fig. 8.** Influence of the thermodesorption temperature on the nitrogen flow inside the ITEX trap.

With a reduced pressure in the vials, we observed that the extraction rate accelerated. For the most volatile compounds, a prolonged extraction time had a negative effect on the recovery of the molecules [1]. Indeed, when extraction time was too long, the most volatile compounds were released from the sorbent. For the majority of the molecules studied in ACM, the results of the experiment showed an optimal time of 30 min at 55 °C. The extraction parameters can be adapted according to the molecules to be studied (Fig. 3).

### 3.1.5. Nitrogen flow desorption

The nitrogen flow was optimized to  $220 \text{ mLmin}^{-1}$  at  $35 \,^{\circ}\text{C}$  to allow for proper desorption of the compounds fixed to the polymer and extraction to counteract against the pressure into the injector during desorption. An exponential decrease in the nitrogen flow rate was noted when the temperature of the trap increased (Fig. 8). A too-high flow (>300 mLmin^{-1}) sometimes clogged the trap by sealing the sorbent material.

### 3.2. Comparison of HS-SPME, HS-ITEX, and DHS-VTT

The results indicate that DHS-VTT clearly improves the extraction of volatile compounds from a complex matrix as the ACM (Table 3). The peak area can be increased by a factor of 450 for some compounds in comparison with using the HS-SPME method. In comparison, HS-SPME extraction, widely used in common headspace applications, achieves lower efficiency for all compounds measured under the same temperature and extraction time conditions. The DHS-VTT technique enriches the gas phase rapidly by limiting the matrix effects because of the reduced pressure in the vial. Moreover, the conventional HS-ITEX method cannot extract the least volatile compounds. The headspace is rapidly in a stable state in HS-ITEX, and the strokes are inadequate to extract more volatile compounds. The choice of polymer in the DHS-VTT extraction trap was also very important for optimal extraction. The best compromise for the 43 compounds used in this study was the Tenax TA/Carbosieve SIII blend.

The profiles of the volatile fraction obtained for a plain yoghurt using the DHS-VTT, HS-ITEX, and HS-SPME extraction methods show that the DHS-VTT method was suitable for this type of sample (Fig. 9). The analyses performed on the yoghurt confirm the results obtained with the ACM. The HS-ITEX method was effective for the extraction of highly volatile compounds such as acetaldehyde but did not extract heavier compounds under the described conditions. With the HS-SPME all compounds except the decanoic acid could be identified. However, the signals were much weaker than with the DHS-VTT method. The surface area of the peaks was higher with DHS-VTT and a higher number of compounds could be detected in SCAN mode using this method.

### 3.3. Performance evaluation of DHS-VTT

Performance evaluation was carried out by determining the following parameters:

• The linearity (*R*<sup>2</sup>) of the method was evaluated by measuring the target compounds in six different concentrations in the ACM corresponding to the ranks commonly found in dairy matrices.



**Fig. 9.** Chromatograms corresponding the volatile fraction of plain yoghurt extracted by DHS-VTT, HS-ITEX and HS-SPME methods. The chromatographic conditions were given in Section 2.2 Instrumentation for GC–MS analysis (sample temperature 55°C, extraction time 30min). Peak numbers correspond to : 1:Acetaldehyde, 2:Acetone, 3:Ethylacetate, 4:Butan-2-one, 5:Butane-2,3-dione, 6:Pentane-2,3-dione, 7:Hexanal, 8:Heptan-2-one, 9:Octanal, 10:3-Hydroxy-butan-2-one, 11:2-Methylpentan-3-ol, 12:2-Hydroxy-3-pentanone, 13:Nonan-2-one, 14:Nonanal, 15:Acetic acid, 16:Propanoic acid, 17:2-Methylpropanoic acid, 18:Undecan-2-one, 19:Butanoic acid, 20:2:Phenylacetaldehyde, 21:Pentanoic acid, 22:Hexanoic acid, 23: 6,10-dimethylundeca-5,9-dien-2-one, 24:2-Phenylethanol, 25:Octanoic acid, 26:Nonanoic acid, 27: δ-Decealactone, 28:Decanoic acid, 29: δ-Dodecalactone, A, Artifact.



Fig. 10. 850 injections of the ACM sample over two weeks in DHS-VTT. Y-axis: Sum of the peak areas of the 43 molecules selected. Standard deviation 9.6%.

The  $R^2$  was approximately 0.99 +/- for all compounds except for  $\gamma$ -butyrolactone with 0.98.

• The MDL of the target molecules was estimated according to the US Environmental Protection Agency procedure and Eq. (1):

$$MDL = t_{(N-1, 1-\alpha=0.99)} \times S_c$$
(1)

- where *t* is the student's *t* value with a confidence level of 99% and six degrees of freedom and  $S_c$  the standard deviation of seven replicates at a concentration level featuring a signal-to-noise ratio (S/N) of three to one. The MDLs measured for alkanes ranged from 0.036 µg L<sup>-1</sup> to 0.822 µg L<sup>-1</sup>, for esters from 0.003 µg L<sup>-1</sup> to 0.071 µg L<sup>-1</sup>, for aldehydes from 0.050 µg L<sup>-1</sup> to 2.89 µg L<sup>-1</sup>, for ketones from 0.145 µg L<sup>-1</sup> to 11.9 µg L<sup>-1</sup>, for lactones from 0.130 µg L<sup>-1</sup> to 0.195 µg L<sup>-1</sup>, for alcohols from 0.032 µg L<sup>-1</sup> to 0.127 µg L<sup>-1</sup>, and for the carboxylic acids from 0.741 µg L<sup>-1</sup> to 104 µg L<sup>-1</sup> (Table 1).
- The reproducibility (RSD%) was obtained by determining the relative standard deviation calculated on the analyses of the samples eight times over a period of two weeks. Reproducibility was measured between 2.2 and 33% for all compounds (Table 1). Reproducibility was low for the carboxylic acids; the extraction conditions were not optimized for these compounds.
- The extraction ratio (*E*) of the method was evaluated by extracting the same sample five times. The *E* value was calculated according to Zimmermann et al., by plotting the logarithmical peak areas against the number of extraction and a simplified Eq. (2) [30]. The slope of the linear regression is represented in the equation by the log (1 E).

$$\log n_{f,x} = \log (n_{s,0}E) + (x-1)\log(1-E)$$
(2)

The *E* value ranged from 1.0% for dodecanoic acid to 77.8% for butan-2-one.

• 850 injections of ACM were made using the same ITEX trap. The results show the reproducibility and stability of the analyses, with a maximum variation of 9.6% between the two extreme results (Fig. 10).

### 4. Conclusions

This newly developed DHS-VTT technique improves the extraction of volatile compounds from an ACM by a simple and inexpensive modification of the autosampler and by using commercial ITEX hardware. Using the principle of DHS-VTT provides a rapid extraction of target compounds with minimal damage to the sample and limited artifact formation. Working at reduced pressure increases the evaporation rate of the compounds. Extraction under continuous reduced pressure avoids creating a system in equilibrium, and, thus, extraction remains dynamic. Our results show good repeatability and sensitivity for the majority of the target molecules assessed.

Comparing the results of extraction by DHS-VTT (TTA, TGR, CSIII, and TTA/CSIII), HS-ITEX (TTA) and HS-SPME (DVB/CAR/PDMS), we observe that DHS-VTT shows benefits for both time and sensitivity of extraction for volatile compounds, including group 1, group 2, and group 3 (Table 3). The much larger amounts of compounds extracted with the DHS-VTT method would facilitate more efficient olfactometric analyses. However, further research is necessary to compare how representative the different extraction methods are for odors to validate the developed method for olfactometry profiling. This would also require detailed odor representativeness studies [31,32].

To the authors' knowledge, no other publication has reported on the development of this new DHS-VTT method, which allows for better extraction of target volatiles using shorter extraction times and lower temperatures.

### Notes

The authors declare no competing financial interest.

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